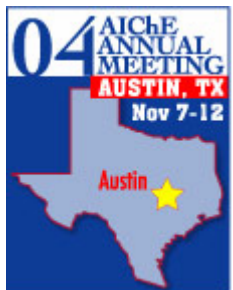


Modeling and control of size distribution for fluidized bed silane decomposition

Christy M. White
B. Erik Ydstie

Department of Chemical Engineering
Carnegie Mellon University
Pittsburgh, PA

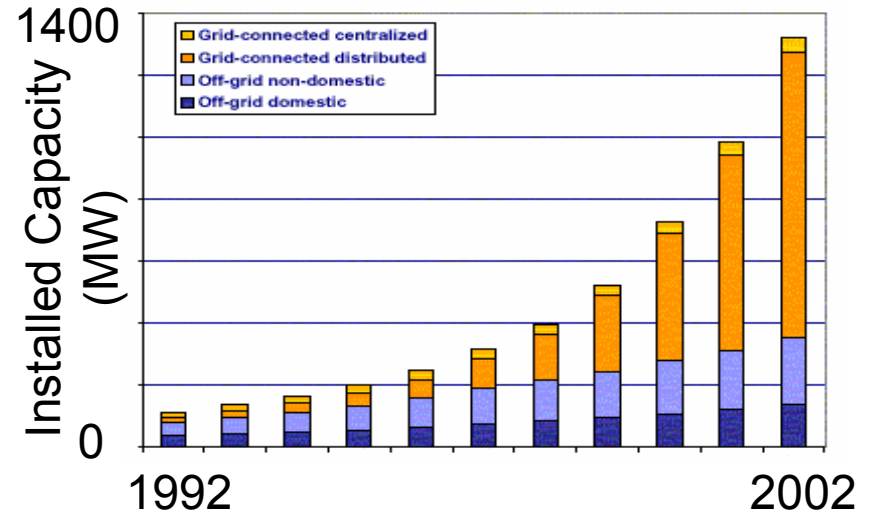




Photovoltaic Industry

Industry Growth

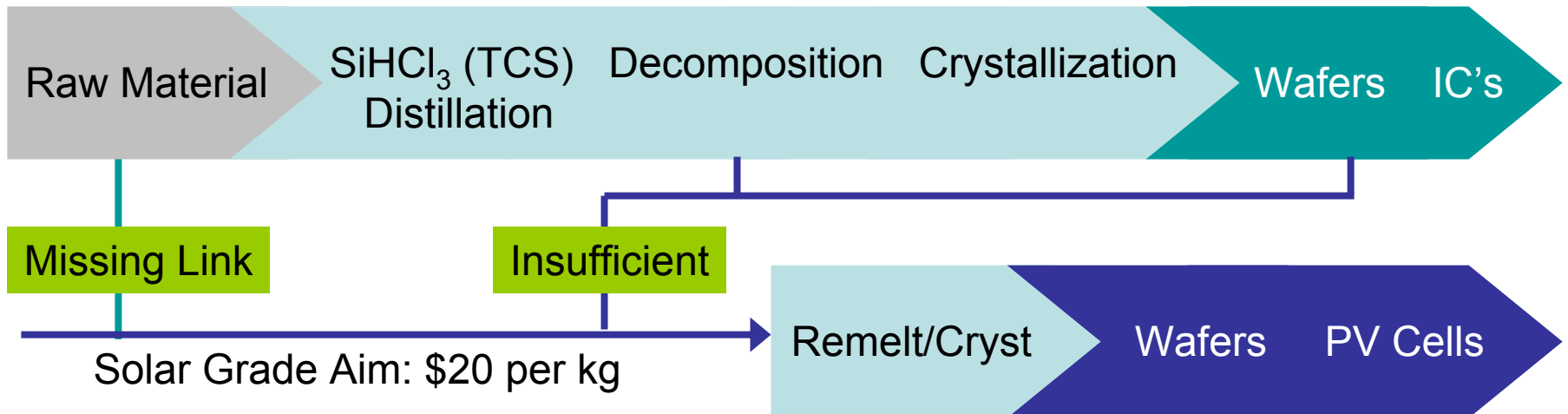
IEA-PVPS, '03



Solar Cell Production

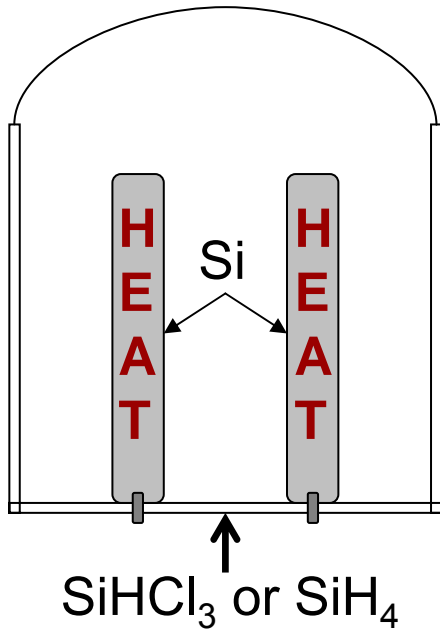
Metallurgical Grade \$3-5 per kg

Electronic Grade \$40-60 per kg

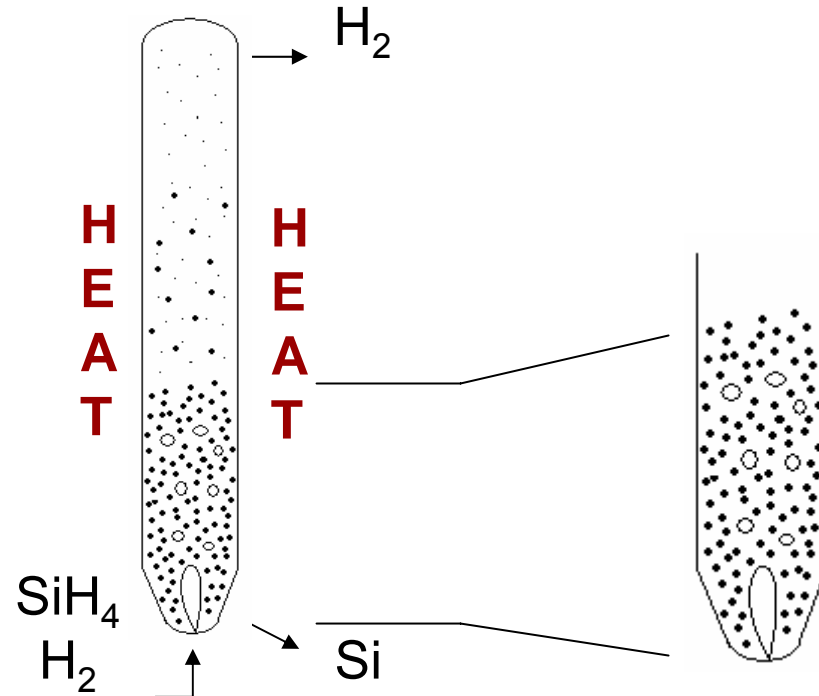




Silicon Production



Siemens Reactor
Batch Process
1100°C

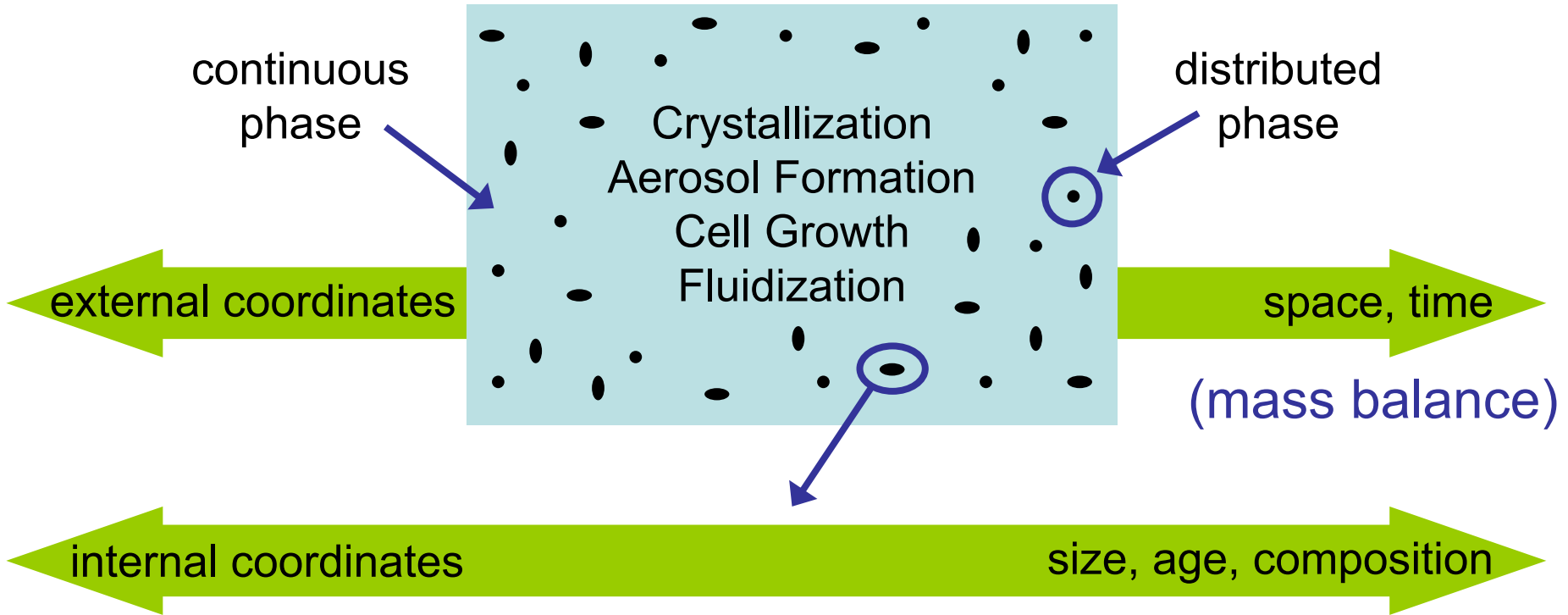


Fluid Bed Reactor
Continuous Process
650°C
Large surface area

Dense Phase
SiH₄ Decomposition
Particle Growth
Size Distribution



Modeling Particulate Processes



Population Balance

$$V \left(\frac{\partial n}{\partial t} + \underbrace{\nabla \cdot \mathbf{v}_i n}_{\text{internal flux}} + \underbrace{D - B}_{\text{death and birth terms}} \right) + n \frac{dV}{dt} = - \sum_k \underbrace{Q_k n_k}_{\text{external flow terms}}$$

density distribution

internal flux

death and birth terms

external flow terms



Overall Reaction and Gas Phase

Thermal Decomposition of Silane: $\text{SiH}_{4(g)} \rightarrow \text{Si}_{(s)} + 2\text{H}_{2(g)}$

Ideal operation: dense zone is a CSTR

Gas phase balance equations (SiH_4 , H_2)

$$\frac{d(V_g \cdot C_{so})}{dt} = F_{in} \cdot C_{si} - F_{out} \cdot C_{so} - (R + \text{loss}_{hom}) \cdot V_g$$

$$\frac{d(V_g \cdot C_{ho})}{dt} = -F_{out} \cdot C_{ho} + 2 \cdot (R + \text{loss}_{hom}) \cdot V_g$$

Reaction rate defined by Lai et al. (1986)

$$R_{het} = 2.79 \times 10^8 \exp(-19530/T) C_s$$

$$R_{hom} = 2 \times 10^{13} \exp(-26000/T) C_s$$

Accounting for loss through entrainment \rightarrow Total reaction:

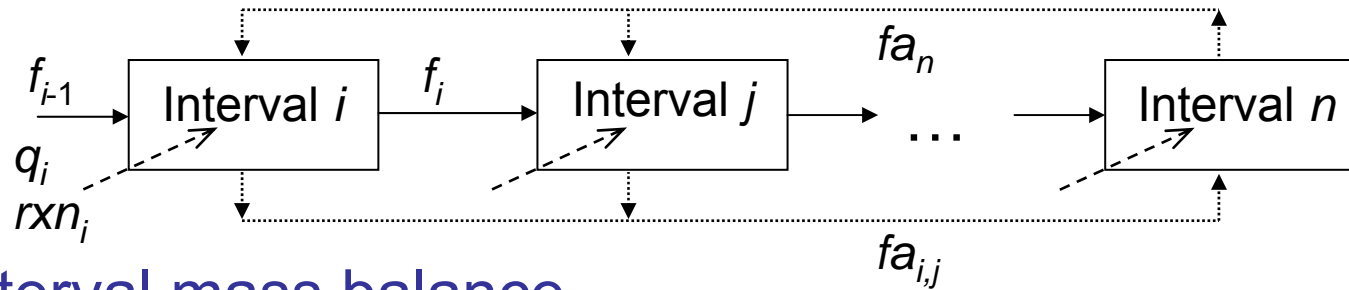
$$R = R_{het} + (1 - \eta) R_{hom}$$

η is fraction of product (powder) lost

Behavior along external coordinate axes: position and time



Solid Phase



Size interval mass balance

$$\frac{dM_i}{dt} = f_{i-1} + rxn_i - f_i + fa_i^{IN} - fa_i^{OUT} + \sum_i q_i$$

Assume

$$rxn_i = R \cdot \frac{A_i}{\sum_i A_i}$$

$$fa_{i,j} = k_{i,j} C_i C_j \Rightarrow$$

$$fa_i^{OUT} = \sum_j \left(fa_{i,j} \cdot \frac{m_i}{m_i + m_j} \right)$$

$$fa_i^{IN} = \sum_j \sum_k fa_{j,k}, \text{ for}$$

$$m_i^{LB} \leq (m_j + m_k) < m_{i+1}^{LB}$$

Derive f_i

assuming continuous number:

$$N_i = \frac{M_i}{m_i} \Rightarrow \frac{dN_i}{dt} = \frac{1}{m_i} \cdot \frac{dM_i}{dt}$$

can obtain:

$$f_i = (rxn_i + aterm_i) \cdot \frac{m_{i+1}}{m_{i+1} - m_i}$$

$$aterm_i = fa_i^{IN} - m_i N_i$$

Behavior along internal coordinate axis: size



Solution Strategy for Discrete Model

Ordinary differential equations for mass in gas and solid phases

+

Algebraic constitutive equations



DAE system solved by MATLAB's ode15s

<i>Adjustable Parameters</i>		<i>Example Values</i>
η	Fraction of powder lost	0 – 1
$k_{i,j}$	Aggregation proportionality constant	0 – 10^{-8} (size dependent)



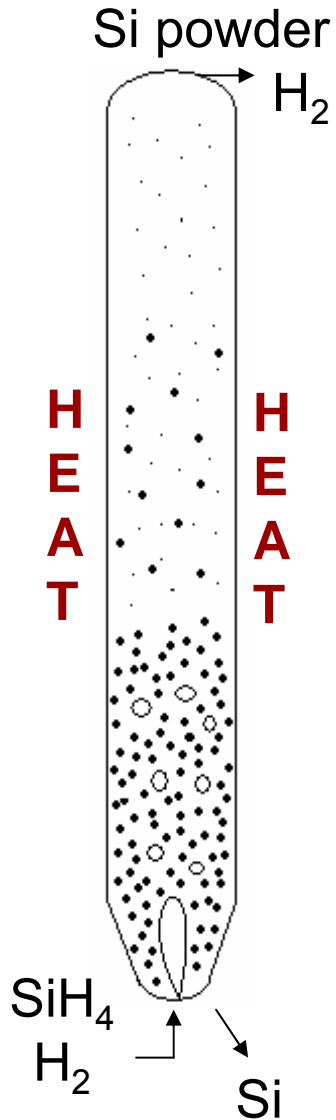
Experimental Data for Validation

Operation of pilot scale reactor

Load known initial distribution
– sieves used to measure distribution

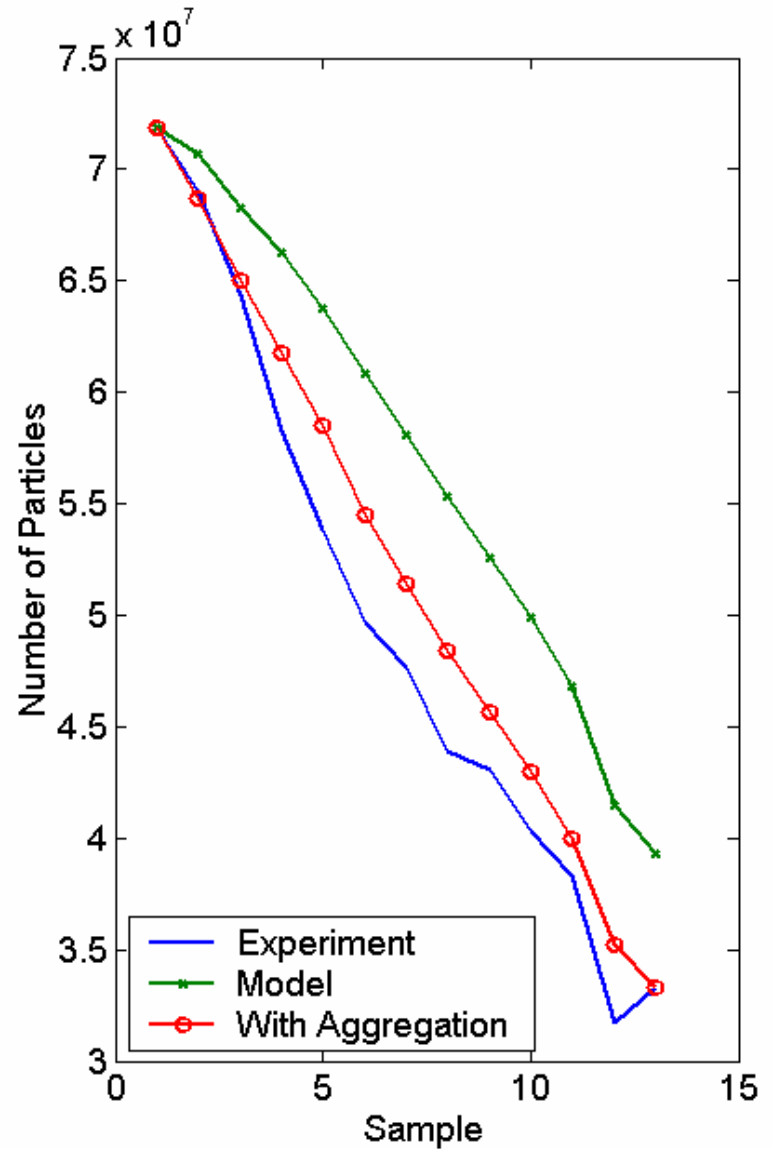
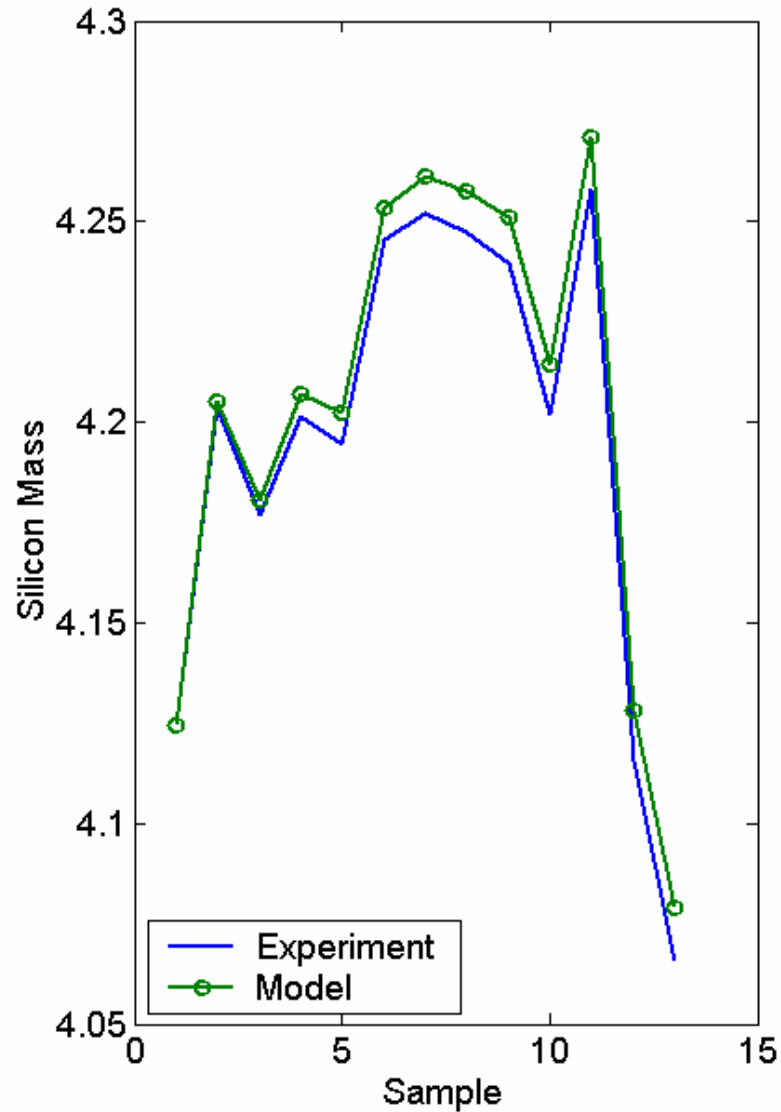
Continuous feed to fluidized bed

Withdraw samples regularly
~8-12 samples per run



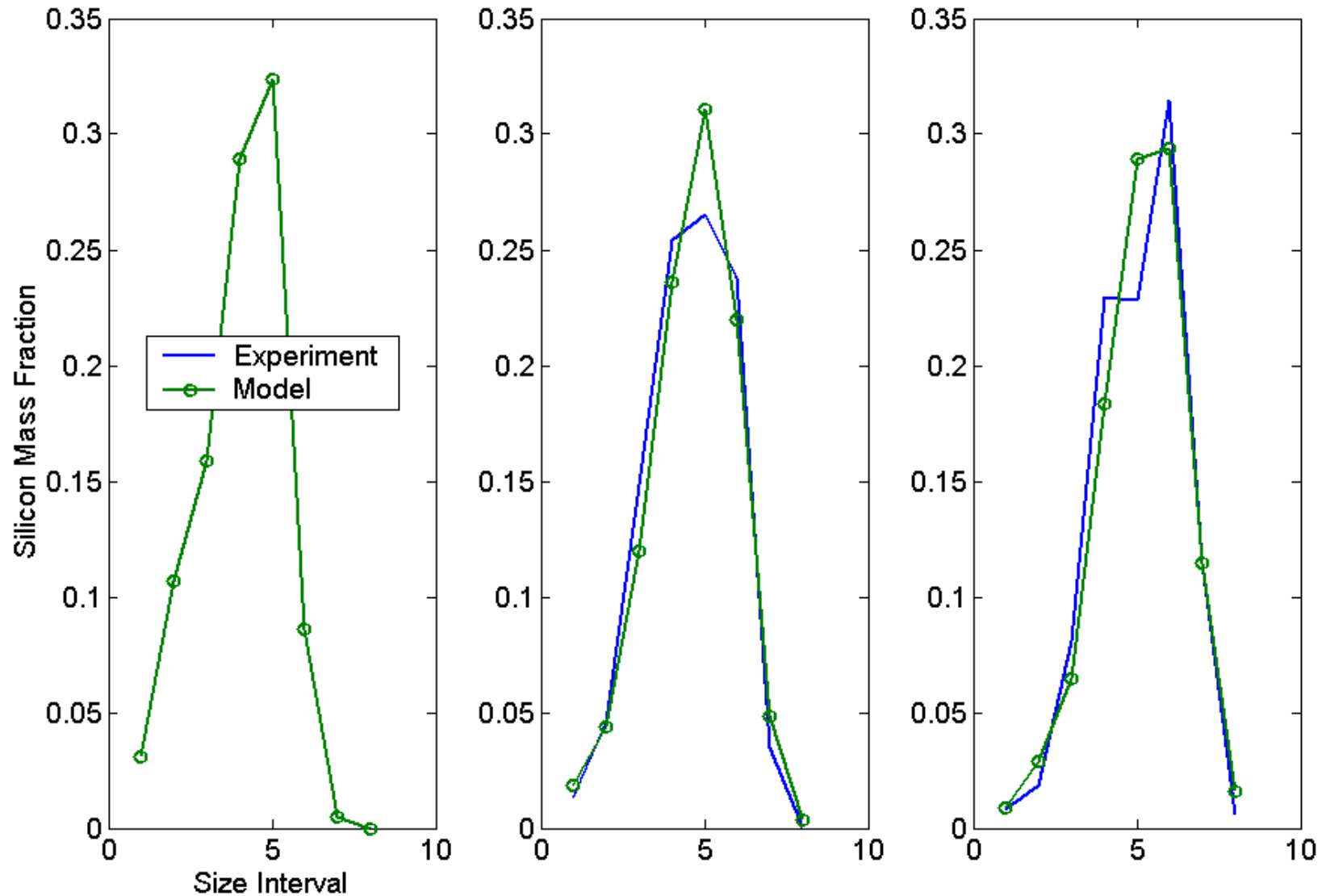


Silicon in Reactor





Particle Size Distribution



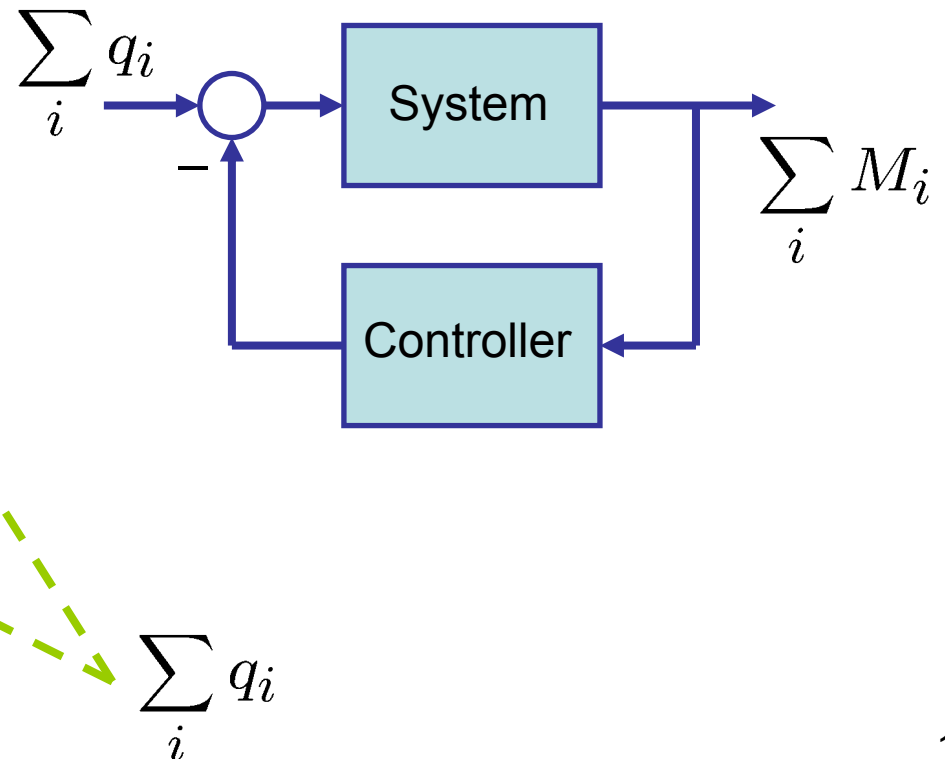
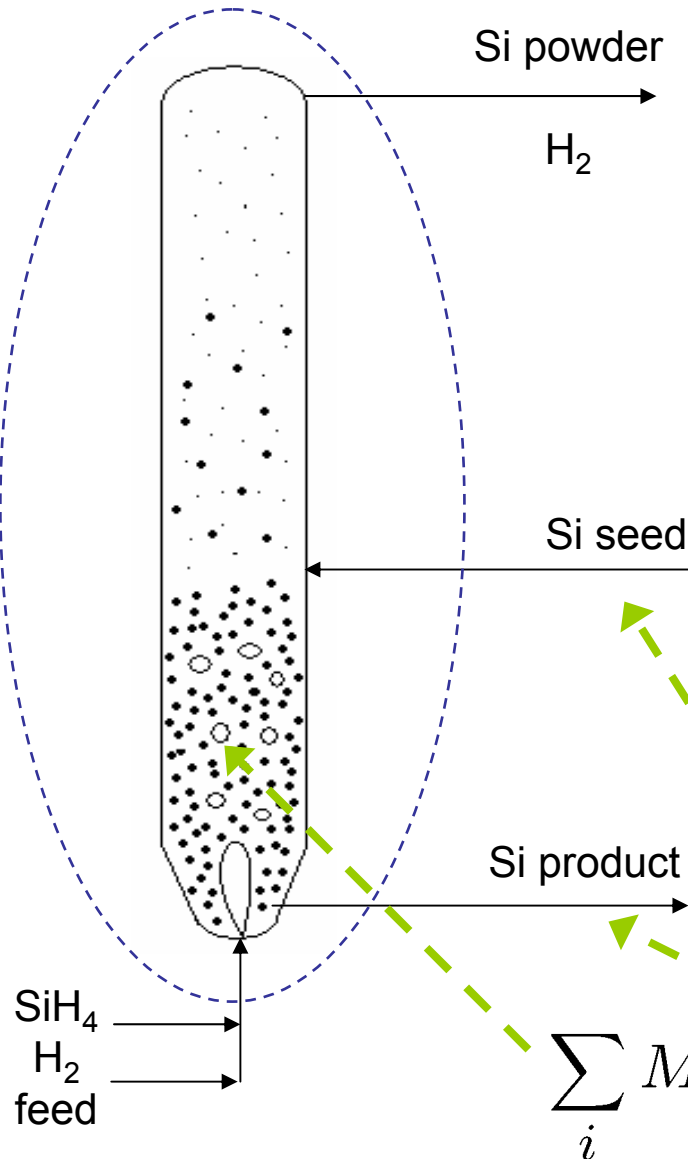


Controlling Continuous Operation

Objective

control: mass of silicon

manipulate: external flow rates





Inventory Control of Population Balance

$$\frac{dM_i}{dt} = \underbrace{f_{i-1} + rxn_i - f_i + fa_i^{IN} - fa_i^{OUT}}_{g_i} + \sum_i q_i$$

Apply inventory control to system:

$$\sum_i \frac{dM_i}{dt} = \sum_i g_i + \sum_i q_i = -K \left(\sum_i M_i - M^* \right)$$

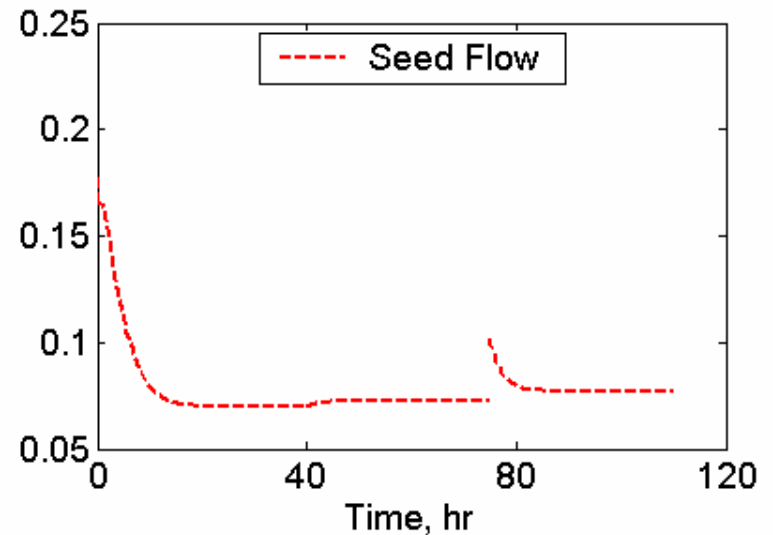
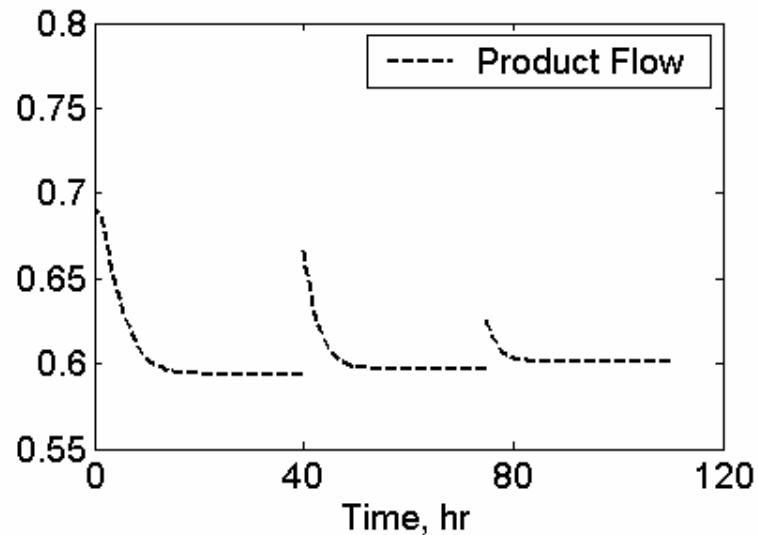
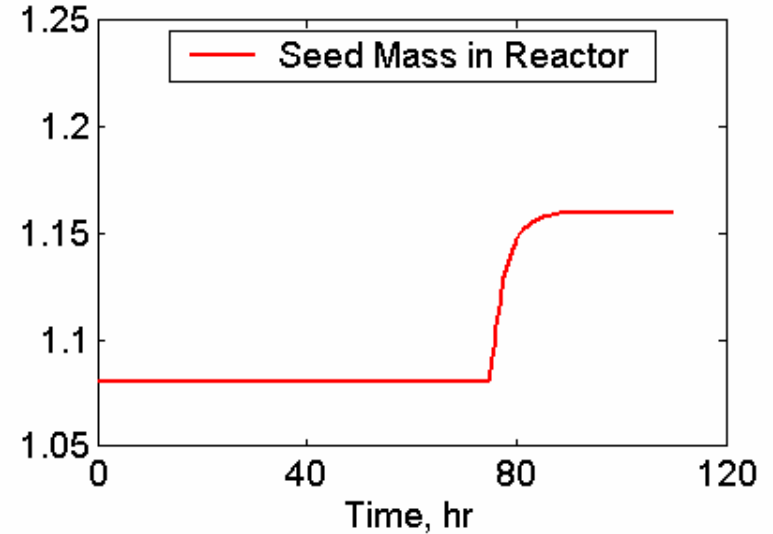
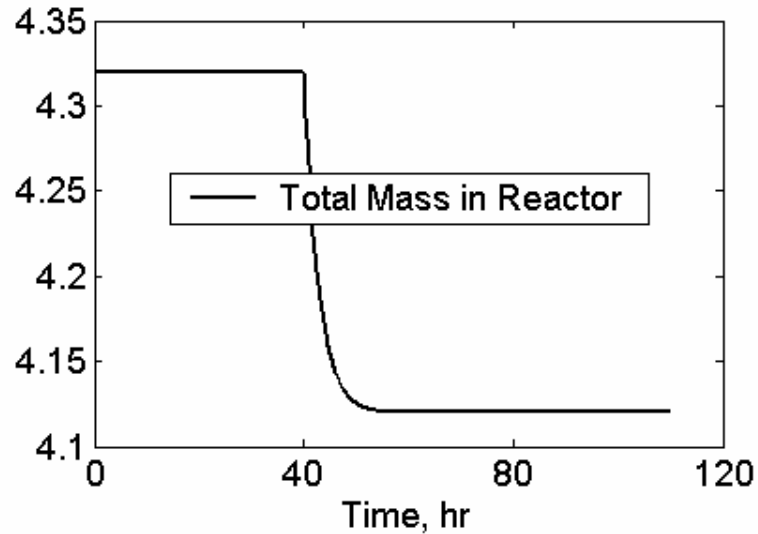
$$\Rightarrow \sum_i q_i = - \sum_i g_i - K \left(\sum_i M_i - M^* \right)$$

Constant mass in reactor: $product = - \sum_{i=1}^N g_i - K \left(\sum_{i=1}^N M_i - M^* \right)$

Constant seed mass: $seed = - \sum_{i=1}^{I_s} g_i - K \left(\sum_{i=1}^{I_s} M_i - M_s^* \right)$

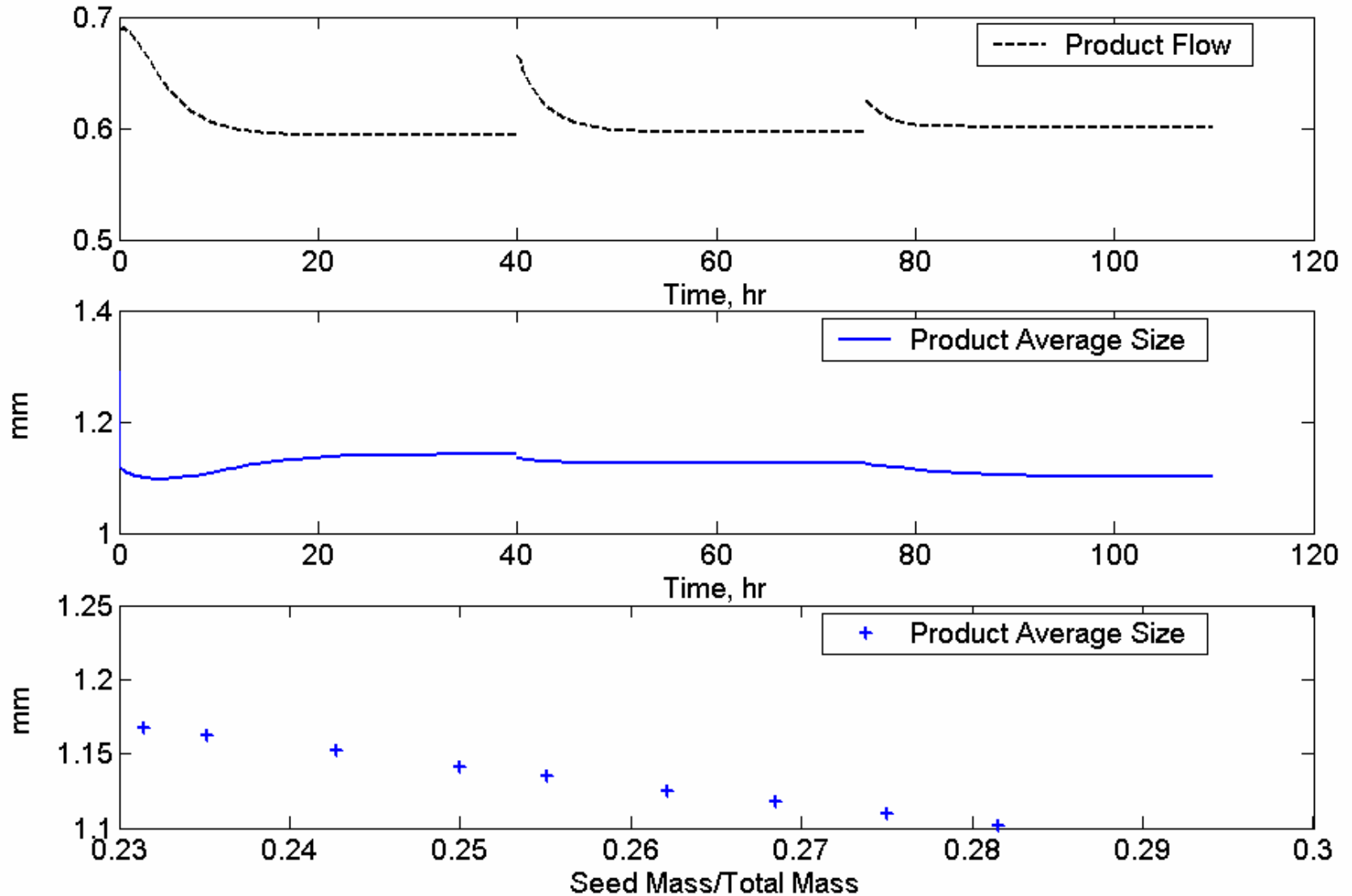


Response to Set Point Changes



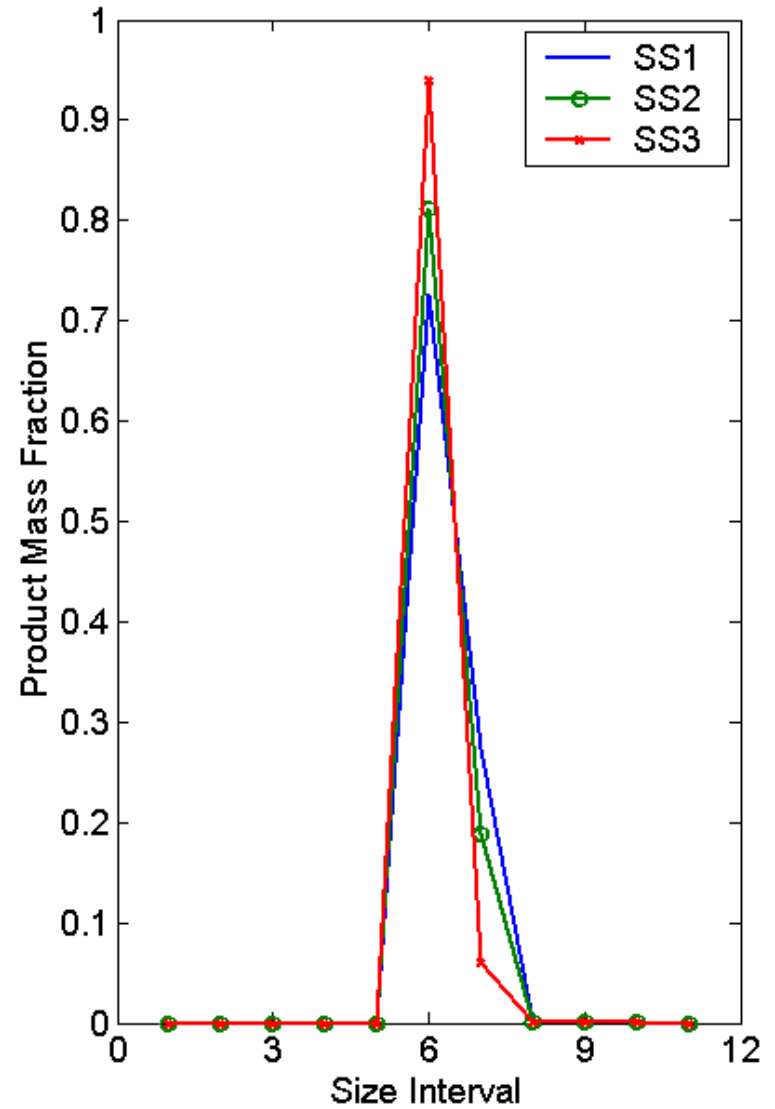
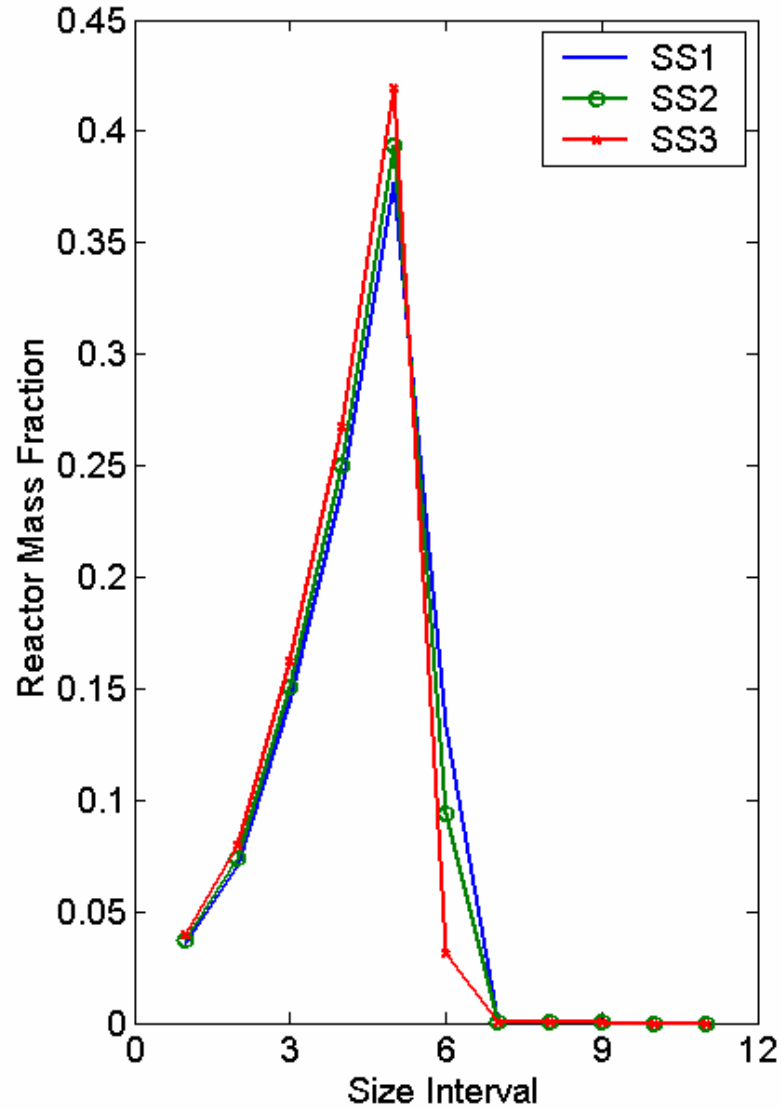


System Dynamics





Silicon Size Distribution





Summary

- Size interval mass balance predictions of particle distribution compare well with data
- Simulations of continuous operation and inventory control indicate that size is controllable
- Further investigate measurability and stability
- Application to other particulate processes or multi-scale modeling is significant



Acknowledgements

- NSF Graduate Research Fellowship Program
- Solar Grade Silicon LLC
- Reactech Process Development Inc.
- Ydstie Research Group

Any opinions, findings, conclusions or recommendations expressed in this publication are those of the author(s) and do not necessarily reflect the views of the National Science Foundation